

A New Viscosity-Surface Correlation for Propane

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 - Problems with consistency
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Motivation – Problems and Tasks

Convenience for engineers

- Use of a Standard Database Program for Thermophysical Properties – consistent with respect to thermodynamic and transport properties: REFPROP¹
- Consistency of the formulations for water:
 - Equation of state (EOS): Wagner and Pruss (2002)²
 - Viscosity η : Huber *et al.* (2009)³
 - Thermal conductivity λ : Huber *et al.* (2012)⁴
- Ethane: EOS, η , λ – inconsistent
 - Problem partly solved → new viscosity-surface correlation: presented at the ECTP Conference in Porto, Portugal, last year
 - Paper submitted to *J. Phys. Chem. Ref. Data*

¹ Lemmon, E. W., Huber, M. L., and McLinden, M. O., Standard Reference Data Program, National Institute of Standards and Technology, Gaithersburg (2013).

² Wagner, W. and Pruss, A., *J. Phys. Chem. Ref. Data* **31**, 387-535 (2002).

³ Huber, M. L., Perkins, R. A., Laesecke, A., Friend, D. G., Sengers, J. V., Assael, M. J., Metaxa, I. M., Vogel, E., Mares, R. and Miyagawa, K., *J. Phys. Chem. Ref. Data* **38**, 101-125 (2009).

⁴ Huber, M. L., Perkins, R. A., Friend, D. G., Sengers, J. V., Assael, M. J., Metaxa, I. M., Miyagawa, K., Hellmann, R. and Vogel, E., *J. Phys. Chem. Ref. Data* **41**, 1-23 (2012).

Problems with consistency

Propane: EOS, η , λ – inconsistent

- Correlations recommended in REFPROP
 - EOS Lemmon *et al.* (2009)⁵
 - η Vogel *et al.* (1998)⁶
 - λ Marsh *et al.* (2002)⁷
- Characterization
 - EOS classical including the critical region, an additional parametric crossover EOS not needed
 - η not including a critical enhancement, but using an old-fashioned classical MBWR
 - λ including a critical enhancement according to a simplified crossover model by Olchoway and Sengers (1988)⁸, but again based on an old-fashioned classical MBWR

⁵ Lemmon, E. W., McLinden, M. O., and Wagner, W., *J. Chem. Eng. Data*, **54**, 3141-3180 (2009).

⁶ Vogel, E., Küchenmeister, C., Bich, E., and Laesecke, A., *J. Phys. Chem. Ref. Data*, **27**, 947-970 (1998).

⁷ Marsh, K., Perkins, R., and Ramires, M. L. V., *J. Chem. Eng. Data*, **47**, 932-940 (2002).

⁸ Olchoway, G. A. and Sengers, J. V., *Phys. Rev. Lett.*, **61**, 15-18 (1988).

Correlation method using structure optimization

Selection criteria

- Combination of different terms
- Requirement of reliable experimental data
- Use of simple functional dependencies, e.g., $\eta = \eta(T, \rho)$
- Viscosity-surface correlation for propane⁹ (2006) of Scalabrin *et al.*
→ not recommended within REFPROP

Procedure

- Evaluation and classification of all available viscosity data
- Selection of terms for the complete fluid range of thermodynamic states including the near-critical region
- Assessment of the resulting correlation using statistical parameters and adequate description of experimental data

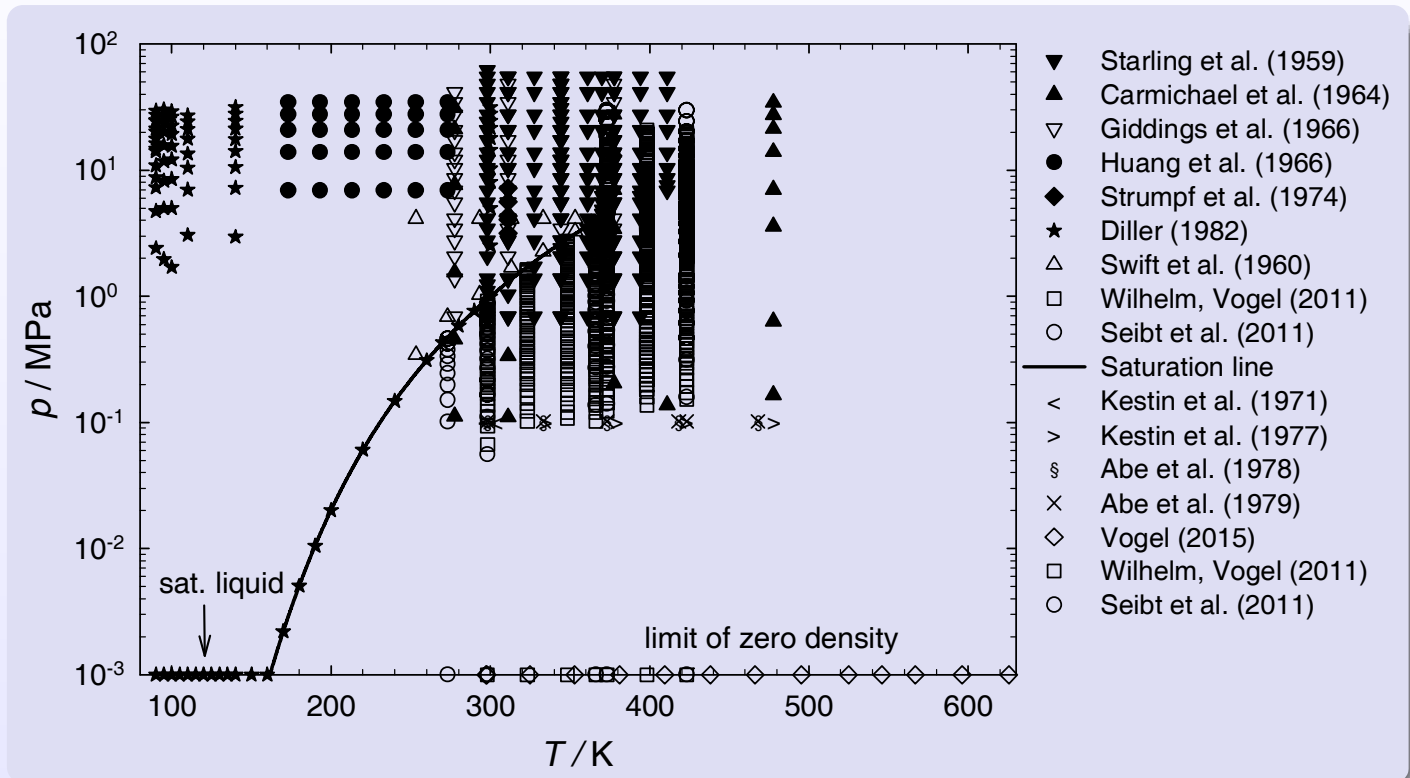
⁹ Scalabrin, G., Marchi, P., and Span, R., *J. Phys. Chem. Ref. Data* **35**, 1415-1442 (2006).

Propane – Primary Experimental Viscosity Data

Authors	Year	Method ¹⁰	Number of points	T K	ρ kg m ⁻³	$\Delta\eta/\eta$ %
Vogel	2015 ¹¹	OD	14	297–625	0	0.3
Wilhelm, Vogel	2011 ¹¹	VW	7	298–423	0	0.3
Seibt <i>et al.</i>	2011	VW	5	273–423	0	0.3
Kestin <i>et al.</i>	1971	OD	2	296–303	2	0.4
Kestin <i>et al.</i>	1977	OD	5	299–478	1–2	0.4–1.0
Abe <i>et al.</i>	1978	OD	5	298–468	1–2	0.4–1.0
Abe <i>et al.</i>	1979	OD	6	298–468	1–2	0.4–1.0
Starling <i>et al.</i>	1959	C	141	298–411	10–578	2.5
Swift <i>et al.</i>	1960	FC	13	243–363	330–566	2.5
Carmichael <i>et al.</i>	1964	RC	22	278–478	2–567	2.5
Giddings <i>et al.</i>	1966	C	74	278–378	10–577	2.5
Huang <i>et al.</i>	1966	FC	30	173–273	540–662	2.5
Strumpf <i>et al.</i>	1974	OQC	5	311	479–491	2.5
Diller	1982	OQC	84	90–300	489–737	2.5
Wilhelm, Vogel	2011 ¹¹	VW	589	298–423	1–447	0.7
Seibt <i>et al.</i>	2011	VW	181	273–423	1–473	0.5

¹⁰ C, capillary; FC, falling cylinder; OD, oscillating disk; OQC, oscillating quartz crystal; RC, rotating cylinder; VW, vibrating wire

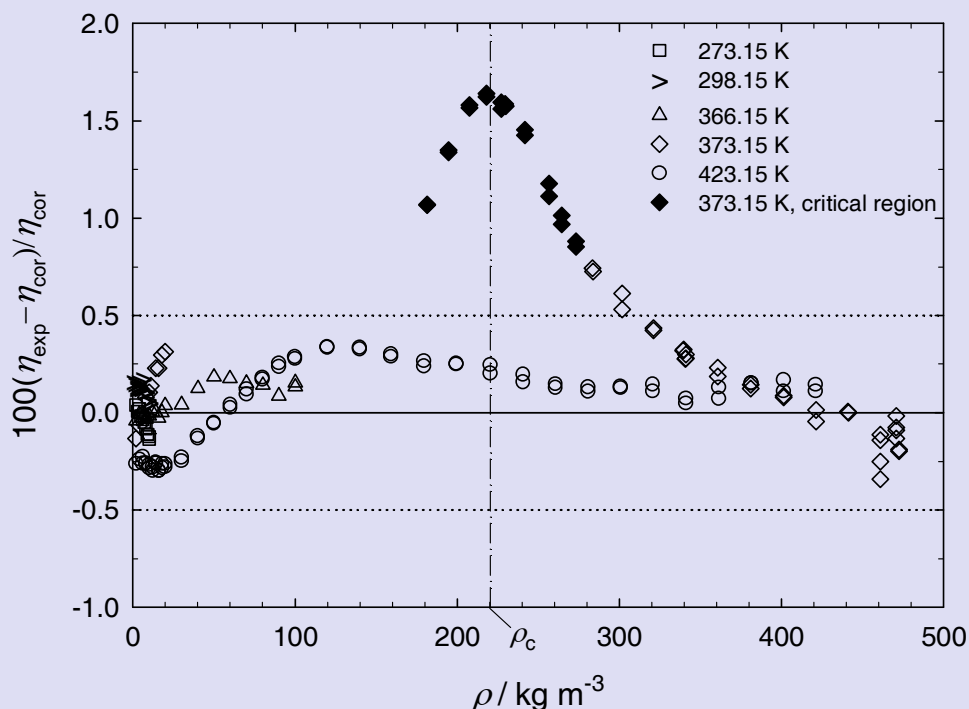
¹¹ re-evaluated data

Propane – p, T diagram with primary experimental data

Propane – Correlation without critical enhancement

New data for propane of Seibt *et al.* (2011)¹²

- Deviations up to +1.64 % near critical density ($\rho_c = 220.478 \text{ kg m}^{-3}$)



¹² Seibt, D., Voß, K., Herrmann, S., Vogel, E., Hassel, E., *J. Chem. Eng. Data*, **56**, 1476-1493 (2011).

Critical enhancement according to Bhattacharjee *et al.* (1981)¹³

- Viscosity η corresponds to an asymptotic power-law divergence:

$$\eta \approx \eta_b (Q_0 \xi)^{z_\eta} .$$

- Critical enhancement represents a multiplicative anomaly:

$$\eta_c = \eta_b [(Q_0 \xi)^{z_\eta} - 1] .$$

- Crossover is needed \rightarrow complete global solution by Olchowy and Sengers (1988) for the mode-coupling theory:

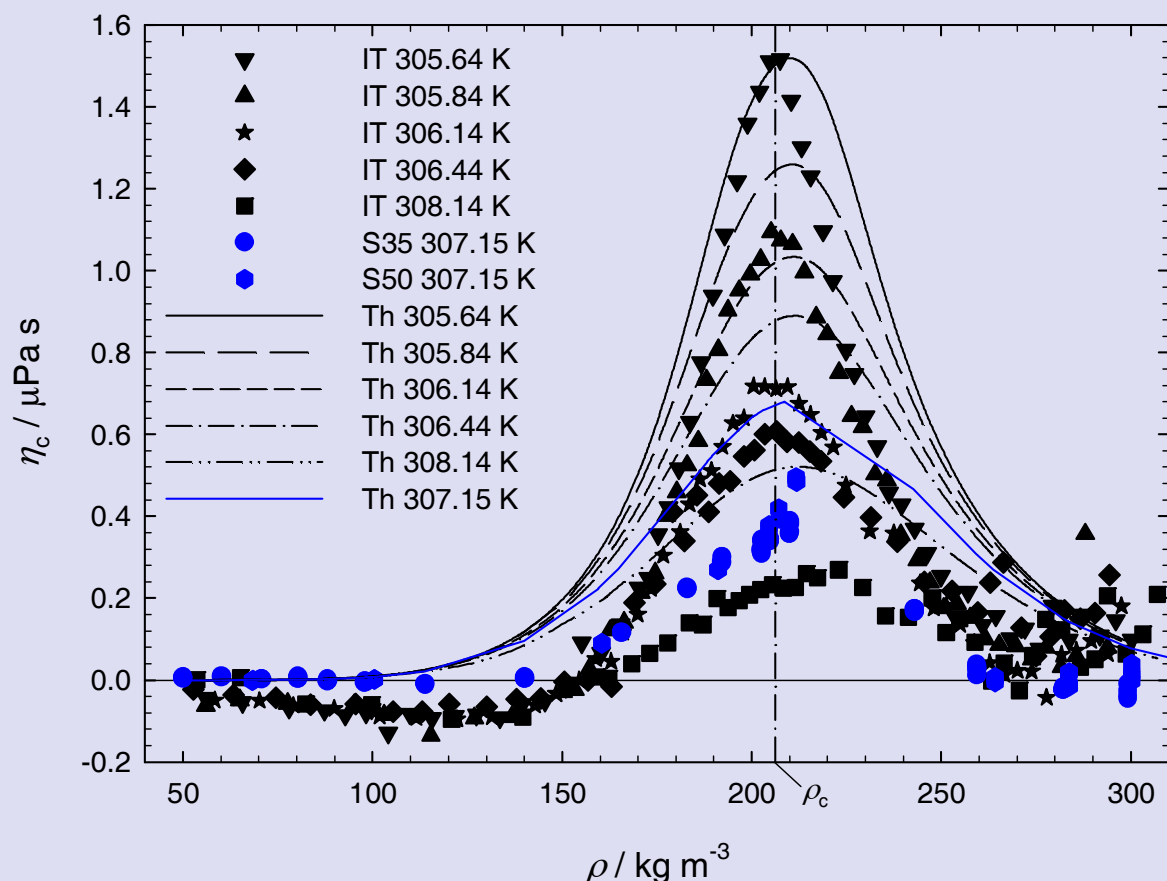
$$\eta_c = \eta_b [\exp(z_\eta H) - 1] .$$

- Simplified closed-form solution earlier developed (Bhattacharjee *et al.*) \rightarrow recently used for IAPWS water (Huber *et al.*, 2009):

$$\eta_c = \eta_b [\exp(z_\eta Y) - 1] .$$

¹³ Bhattacharjee, J. K., Ferrell, R. A., Basu, R. S., and Sengers, J. V., *Phys. Rev. A* **24**, 1469-1475 (1981).

Critical enhancement – ethane: theory vs. experiment



Viscosity-surface correlation for propane

- Reduced quantities: $\tau = \frac{T_c}{T}$, $\delta = \frac{\rho}{\rho_c}$
- Bank of terms for separate zero-density viscosity correlation:

$$\frac{\eta_{0,\text{bank}}(T)}{\mu\text{Pa s}} = \sum_{i=0}^{-8} A_{0,i} \tau^i \quad \text{Result: } A_{0,-1} \text{ and } A_{0,-4}.$$

- Bank of terms for the total correlation:

$$\frac{\eta_{\text{bank}}(T, \rho)}{\mu\text{Pa s}} = \frac{\eta_0(T)}{\mu\text{Pa s}} A_0 + \sum_{i=0}^8 \sum_{j=1}^{20} A_{ij} \tau^i \delta^j + \sum_{k=0}^5 \sum_{l=1}^5 A_{kl} \tau^k \delta^l e^{-\delta} + \sum_{m=0}^1 A_m \tau \delta \mu_m e^{-\beta_m(\delta-\gamma_m)^2 - \varepsilon_m |\tau - \zeta_m|}.$$

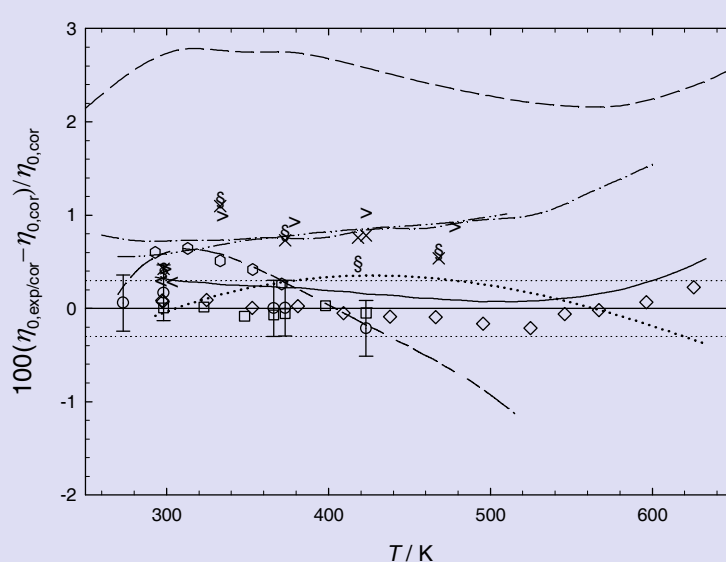
- Result for propane:

$$\frac{\eta_{\text{cor}, \text{C}_3\text{H}_8}(T, \rho)}{\mu\text{Pa s}} = \sum_{i=1}^{12} A_i \tau^{t_i} \delta^{d_i} + A_{13} \tau^{t_{13}} \delta^{d_{13}} e^{-\delta} + \sum_{i=14}^{15} A_i \tau \delta e^{-\beta_i(\delta-1)^2 - \varepsilon_i |\tau-1|}.$$

Comparison equation - experiment

Viscosity in the limit of zero density

- Agreement within the experimental uncertainty
- Error bars: $\pm 0.3\%$



◇, □, ○ experimental data in the limit of zero density

<, >, §, × experimental data at atmospheric pressure

⊞ secondary exp. data at atmospheric pressure

— — — Tanaka, Makita (1975)

- · · - Holland *et al.* (1979)

- - - Tarzimanov *et al.* (1987)

- · · - Younglove, Ely (1987)

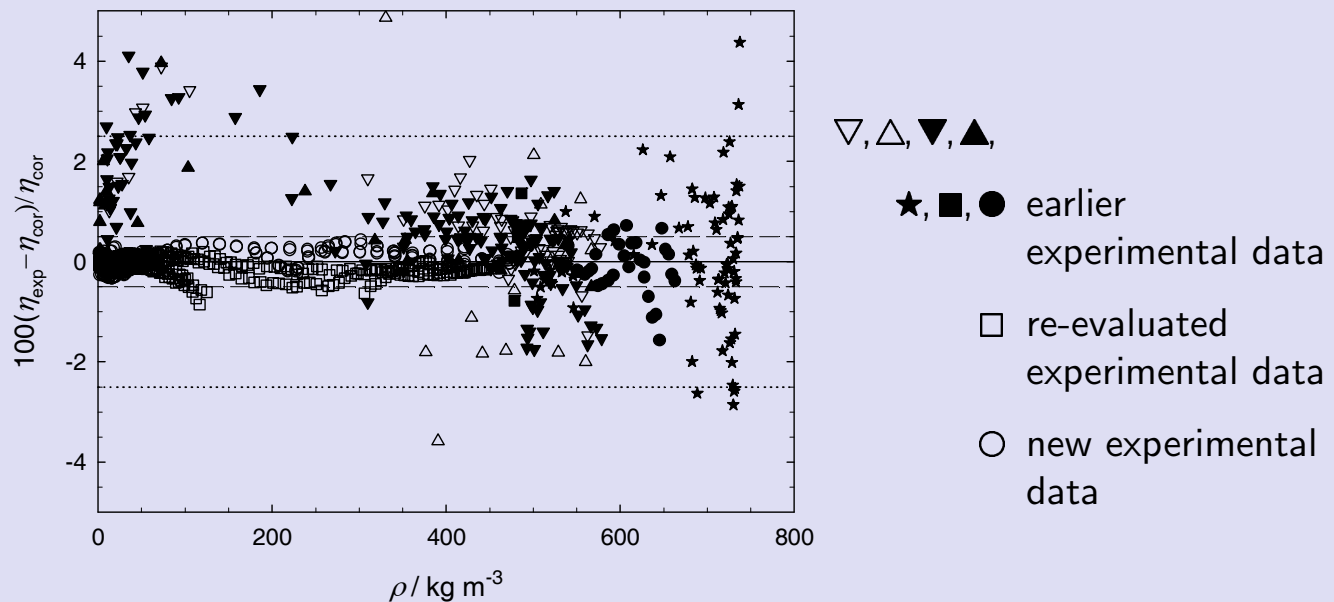
— — — Vogel *et al.* (1998)

· · · Scalabrin *et al.* (2006)

Comparison equation - experiment

Viscosity in the fluid region

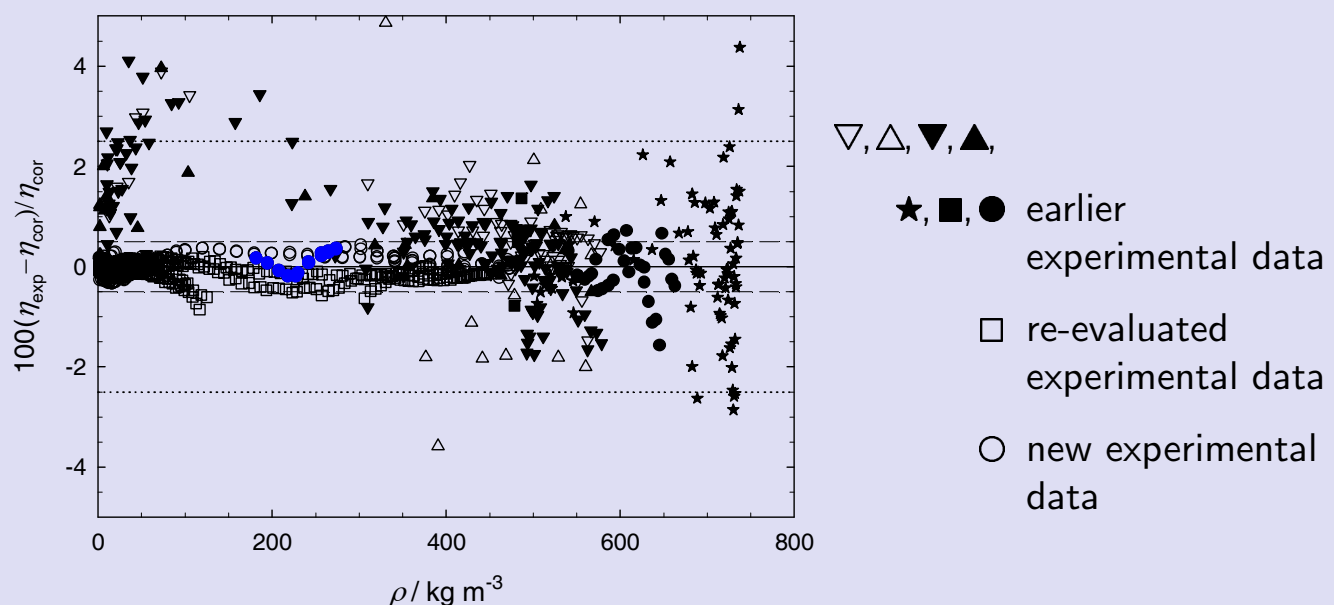
- New and re-evaluated data dominant
- Large deviations at small and high densities for earlier primary data
- Deviations of data in the near critical region $< \pm 0.35\%$



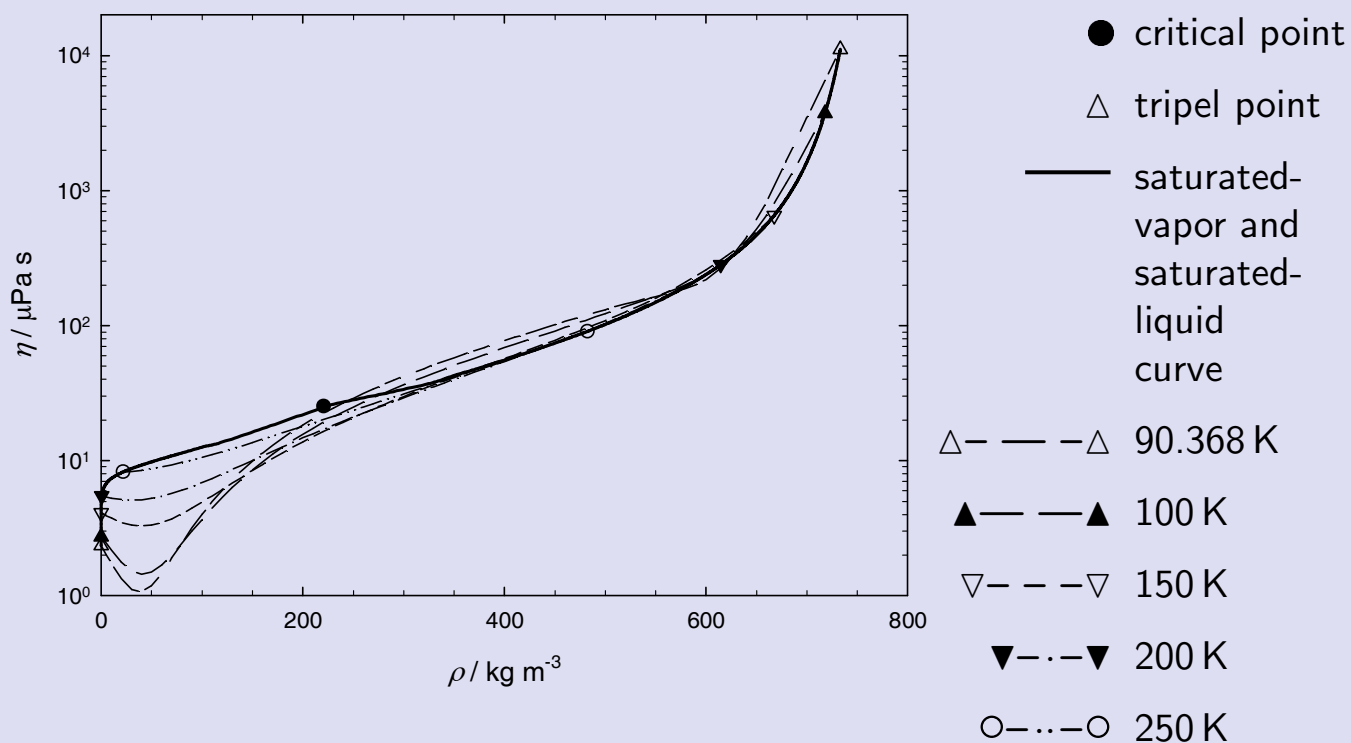
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Viscosity in the fluid region

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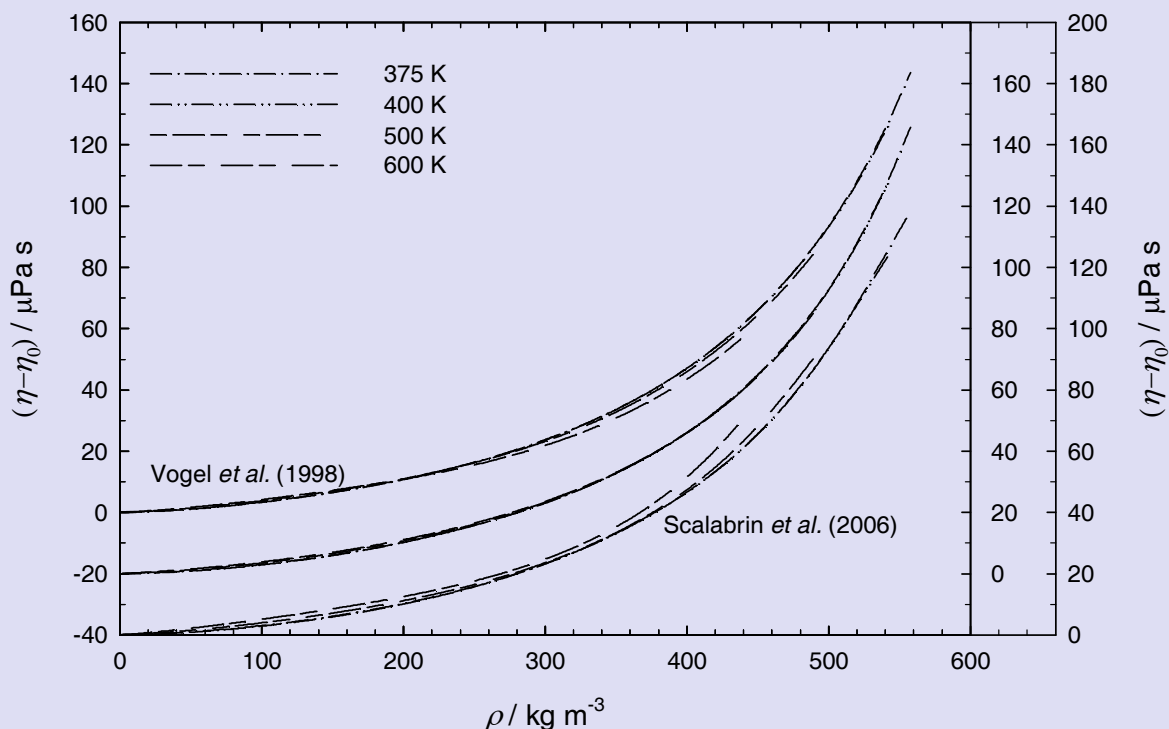


Propane – Correlation in the two-phase region



Propane – Consistency test using behavior of η_{Res}

Comparison to viscosity-surface correlations from literature:
 Vogel *et al.* (1998) and Scalabrin *et al.* (2006)



Conclusion and Outlook

- New viscosity-surface correlation was generated for propane based on new precise experimental viscosity data
- The structure-optimization method of Setzmann and Wagner (Ruhr-Universität Bochum) was used
- The viscosity was correlated as $\eta(T, \rho)$
- Critical enhancement was included using new data of Seibt *et al.*
Theory: divergence at the critical point
Correlation: finite values when approaching the critical point due to used experimental data from the near-critical region

- Further work on n-butane and isobutane

→ precise data using the vibrating-wire viscometer are available for these fluids

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